- 1 In Vitro Electrically Controlled Amoxicillin Release from 3D-printed Chitosan/Bismuth
- 2 ferrite Scaffolds
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21 Abstract

22 The goal of this study was to design and fabricate a 3D-printed wound dressing using chitosan

as a bioink, with the ability to release the antibiotic drug amoxicillin (AMX) in response to mild

electrical stimulation. This was achieved through the incorporation of bismuth ferrite (BFO)

25 nanoparticles, which have both magnetic and ferroelectric properties. The chitosan-based

scaffolds containing various concentrations of BFO were analyzed using Fourier transform

27 infrared spectroscopy, and the release of AMX from the scaffolds was evaluated in vitro under

28 electrical stimulation. The results demonstrated that the scaffolds had a suitable structure for

drug loading and release, and the release of AMX was successfully controlled by the applied

30 electrical stimulus. The maximum tensile strength (4.97 ± 0.34 MPa) was observed at the ratio

31 of 6% CHT/0.025% BFO scaffolds and the scaffold with 6% CHT/0.075% BFO had the

32 maximum cell viability of $(\sim 130\%)$ at 168h incubation time. This study highlights the potential

of BFO to deliver therapeutic drugs from a 3D-printed chitosan scaffold in a controlled manner.

- 34 Keywords: Amoxicillin; bismuth ferrite; chitosan; controlled drug delivery; scaffold; 3D
- 35 printing.



38 **1. Introduction**

Designing a wound dressing for use in skin tissue engineering requires detailed optimization of 39 40 its properties considering the extent, shape, and pathophysiology of the injury. A wound dress 41 must provide a moist environment, as well as allow gas exchange and be mechanically compatible with the native skin tissue. Besides, additional therapeutics could be required at the 42 site of injury caused by burns, trauma, or surgical operations. Wound dressings with porous 43 architecture can be designed to carry such therapeutic drugs to the desired area, promoting 44 45 healing while favoring cell attachment, proliferation, and tissue formation. One such method involves using three-dimensional (3D) printing technology to fabricate structures with custom 46 47 internal micro-architecture [1]. This technology incorporates novel materials (i.e. natural or synthetic) in the design of cell-laden bioinks which can contain drug substances to promote 48 49 wound treatment and management. The versatility and repeatability provided by 3D printing technology allow us to overcome the shortcomings of traditional biofabrication methods. 50 Three-dimensional scaffolds comprised of artificial and organic polymers have been created 51

52 using a variety of techniques, including gas foaming, melt molding, electrospinning, and phase 53 separation. Nevertheless, these scaffold production techniques cannot precisely alter the 54 scaffold's shape, inner channel arrangement, or pore size. The severe processing conditions of 55 these approaches also prevent the production of scaffolds containing cells [2].

The technology also facilitates the 3D-printed of skin and the engineering of skin substitutes or 56 scaffolds that allow drug loading [3]. The development of magnetically responsive scaffolds is 57 58 based on the blending of polymer gels with magnetic nanoparticles, enabling the modulation of drug and cell delivery at the target wound area [3]. Bismuth ferrite (BFO), a multiferroic 59 material with both magnetic and ferroelectric properties at room temperature, can be formed as 60 61 a drug carrier whose release profile could be controlled with electrical induction [4]. Controlled 62 release and targeted delivery of drugs reduce the side effects that can arise from excessive use while providing a sustained release of drugs. Due to the ongoing emergence of bacterial 63 64 resistance, numerous studies on the subject of antimicrobial studies in metal-based NPs are 65 crucial to nanomedicine. The compounds with bismuth ferrite nanoparticles can increase activity by adding additional materials. Many studies have reported the associated antibacterial 66 activity of BFO nanoparticles that is size/shape dependent [5]. A recent study shows that the 67 antibacterial activity of amoxicillin (AMX), one of the most commonly used antibacterial drugs, 68 69 could be maintained for at least 6 weeks using a novel controlled drug delivery system for skin tissue [6]. Our paper demonstrates the feasibility of controlling the release of AMX from BFO 70 nanoparticles in vitro by electricity. 71

For the engineering of skin tissue, natural hydrogels are generally preferred due to their ability to maintain a moist environment while supporting the cells that would regenerate the tissue. Chitosan (CHT) is a natural polymer that can be obtained by partial deacetylation of chitin from sea crustaceans. It is biocompatible and non-allergic, and it can absorb water up to 3 times its weight [7], making it one of the most commonly preferred hydrogel bioink for 3D printing in soft tissue engineering studies. Moreover, chitosan is highly effective in wound healing as it
speeds up tissue formation, [8] and research shows that low molecular weight chitosan prevents
microbial growth by inhibiting bacterial gene expression [9].

Herein, the aim of this article is to develop chitosan-based wound dressing materials that carry 80 81 drugs that can be triggered electrically. Wound dressing materials containing BFO-AMX 82 nanoparticles in different proportions were produced using a 3d printer. Electrically triggered drug release has the potential to create a new perspective for regeneration. In addition, these 83 scaffolds can be used according to the needs of the patient and contribute to the personalized 84 85 treatment method. With the ability to adjust the delivery rate in accordance with the patient's needs, the electrically triggered delivery of AMX from CHT/BFO scaffolds may open up new 86 possibilities for regeneration as well as the individualized therapy of many diseases. To our 87 knowledge, this study is the first to investigate the effect of BFO nanoparticles on AMX release 88 from 3D-printed chitosan-based scaffolds via mild electrical stimulation. The main novelty of 89 90 this study is due to the presence of BFO and the encapsulation of the drug into the BFO at the 91 synthesis stage. In addition, these drug encapsulated particle was added into the CHT scaffold to observe the release control with both the degradation of CHT and electric stimulation. There 92 93 are some studies about the investigation of electric stimulation to drug release [10, 11] but fabrication of AMX encapsulated BFO and BFO-added 3D-printed CHT scaffolds are the new 94 95 study for the literature. After the fabrication process, the chemical, morphological, mechanical and thermal characteristics of the scaffolds were investigated. Then, electrical drug release and 96 97 cell biocompatibility were investigated by in vitro studies.

98 2. Materials and Methods

99 **2.1. Materials**

Bismuth (III) nitrate (Bi₅O(OH)₉(NO₃)₄, MW=1.461,99 g/mol), iron (III) nitrate nonahydrate
(Fe(NO₃)₃, MW=403.95 g/mol), dichloromethane (DCM), and nitric acid (65%) were

102 purchased from Merck KGaA, Germany. Ammonia solution (25%, MW=35.05 g/mol) was 103 supplied from ISOLAB (Wertheim, Germany). Chitosan (low molecular weight, deacetylated 104 chitin) was purchased from Sigma Aldrich (USA). Acetic acid glacial (CH₃COOH, M = 60.05 105 g/mol) was obtained by Merck, Germany, and amoxicillin (96%) was supplied from Acros 106 Organics.

107 2.2. BFO Synthesis

108 BFO nanoparticles were obtained using a co-precipitation route method. Firstly, 2.58 g iron nitride [Fe (NO₃)₃·9H₂O] was dissolved in the distilled water (10 ml) at the magnetic stirrer at 109 300 rpm for 15 min. Then, 1.86 g bismuth nitride (Bi (NO₃)₃.5H₂0) was dissolved in the 10 ml 110 111 nitric acid for half an hour at the stirrer with the same rpm. The two solutions were dissolved 112 entirely and stirred in the same beaker for 15 min to obtain a homogeneous mixture. In this step, 20 mg of AMX was added to this mixture to get drug-loaded BFO nanoparticles. When the 113 mixture reached transparency, an ammonia solution was added to the mixture to control the pH 114 to obtain a precipitate. The preparation of the precursor and co-precipitation solutions was 115 performed at room temperature. The resulting precipitate was passed through the filter paper 116 and washed with distilled water to remove the toxic effect of the agents. Then, the powders 117 were put in the oven for 24 h at 100 °C to evaporate the water in them [12]. 118

119 **2.3. Preparation of the Solutions**

120 6% chitosan (w/v) was dissolved in 2% acetic acid aqueous solution at 80 degrees in a magnetic 121 stirrer for 30 mins [13]. After completely dissolving chitosan, drug-loaded BFO particles were 122 added to the solution at ratios 0.025%, 0.05%, and 0.075%, respectively. The solutions were 123 ready for the 3D printing process.

124 **2.4. Fabrication of the 3D Printed Scaffolds**

125 The scaffold was designed using CAD software. The 3D scaffolds were fabricated using a 3D

126 printer device (Hyrel 3D, SDS-5 Extruder, GA, USA). Hydrogels were loaded into a 10 mL

syringe. The syringe was connected to the 30 Ga needle and placed on the head of the printer.
3D printing was performed at a printing speed of 10 mm/s, the flow rate of 1 ml/h. The scaffold
had a square shape of 20 mm x 20 mm x 1 mm dimensions. The other parameters were set as
follows: the infill density = 60%, the total layer = 8, and the infill pattern was rectangular. At
the end of the printing process, all scaffolds were put in sodium 8% NaOH solution for 5
minutes for crosslinking.

133 **2.5.** Characterization of the Scaffolds

134 2.5.1. Fourier Transform Infrared Spectroscopy (FT-IR)

The molecular structures of the scaffolds were analyzed by using Fourier transform infrared spectroscopy (FTIR, 4700 Jasco, Japan). The results of the spectrum were analyzed at a scanning range of 450-4000 cm⁻¹ and a resolution of 4 cm⁻¹.

138 2.5.2. Scanning Electron Microscopy (SEM) and Transmission Electron Microscope 139 (TEM)

BFO powder was dissolved in methanol using a sonicator to prepare samples for TEM
(HITACHI HT7800), which were then placed onto copper grids covered in carbon. The
morphological analysis of the scaffolds was examined using SEM (EVA MA 10, ZEISS, USA).
The surface of the scaffolds was coated with Au with a coating machine (Quorum SC7620,
ABD). The average pore sizes of scaffolds were measured using software (Analysis5, Olympus,
USA).

146 2.5.3. Differential Scanning Calorimeter (DSC)

The thermal properties of the 3D-printed scaffolds were determined by using a DSC (Shimadzu
DSC 60 Plus, Japan). The temperature ranges were adjusted from 25 °C to 600 °C at the
scanning rate of 10°C/min.

150 **2.5.4. Mechanical Properties of the Scaffolds**

151 The tensile properties of the scaffolds were analyzed using a tensile test machine (SHIMADZU,

152 EZ-LX, CHINA). Before the tensile test, the thickness of the scaffolds was measured using a

153 digital micrometer (Mitutoyo MTI Corp., USA).

154 **2.5.5. X-Ray Diffraction (XRD)**

155 XRD machine was used to obtain the crystal structure of BFO powders and 3D-printed 156 scaffolds. In this test, Cu source (λ =1.54060 A°) was used to obtain the X-rays. The scan range 157 was adjusted to 10 to 90 ° and the scan rate was adjusted to 2°/min.

158 2.5.6. Cell Viability Analysis and SEM Imaging of Cell-Seeded Scaffolds

For the analysis of cytotoxicity of scaffolds on mouse embryonic fibroblasts (NIH 3T3) MTT 159 160 assay was performed on days 1, 4, and 7 of cell culture. Prior to cell seeding, the scaffolds were 161 transferred to 96-well plates and sterilized with ethanol, and then washed with PBS and finally with culture media. Fibroblasts were seeded with a density of 10000 cells/scaffold in a 96-well 162 plate. After 24, 96, and 168 hours of cell seeding, cell viability analysis was carried out 163 according to the manufacturer's protocol. Briefly, the culture media of the samples were 164 replaced with fresh media containing 5 mg/mL MTT (Vybrant MTT Cell Proliferation Assay 165 Kit, Thermo Fischer Scientific), and then the samples were incubated for 4 hours in a CO₂ 166 167 incubator. To dissolve the formazan crystals formed as the reduction of MTT after 4h-168 incubation, sodium dodecyl sulfate (SDS) was added into each well and incubated at 37 °C for 12 hours. The optical density of each sample was measured at 570 and 630 nm by using a 169 microplate reader (Biotek, Winooski, VT, USA). The experiment was performed three times 170 171 (n=3). Percent cell viability was calculated using the following formula (1).

172

Cell Viability (%) = (OD test/OD control) \times 100 (1)

The morphology of the cells on the scaffolds was examined by SEM. The cell-seeded scaffolds
were washed with cacodylate buffer (0.1 M, pH 7.4) and then fixed with 4% glutaraldehyde.
Dehydration was performed with serial dilutions of ethanol. Finally, scaffolds were air-dried

and then coated with gold for 20 s prior to SEM analysis. The attachment and viability of fibroblast cells on the scaffolds were examined by acridine orange staining. After 1, 4, and 7 days of incubation, the growth medium of the cells was removed and the medium was cleaned with PBS. Then, the scaffolds were fixed with 4% paraformaldehyde for 30 minutes at room temperature and washed with PBS. After cleaning with PBS, $6 \mu g/ml$ acridine orange was added to each scaffold and incubated at room temperature for 10 minutes. Then, the acridine orange solution was discarded and the scaffolds were washed three times with PBS.

183 2.5.7. Drug Release Behavior of the AMX from the Scaffolds

The AMX release from the scaffolds was examined in phosphate-buffered saline (PBS, pH:7.4) 184 185 at 37°C. The resultant AMX concentration was detected with a UV-Vis spectrophotometer (Shimadzu, Tokyo, Japan) at various time intervals. The calibration curve of the AMX was 186 determined over a wavelength range of 190-500 nm and five different AMX concentrations 187 (0.25, 0.5, 1, 1.5, and 2 µg/ml). In the drug release test, firstly 5 mg of AMX-loaded scaffolds 188 were weighed and dissolved with 1 ml PBS (pH:7.4) in Eppendorf tubes. The absorbance values 189 of the AMX were detected at different time intervals. Fresh PBS was used after each 190 measurement. The AMX release was determined at 230 nm. 191

192 2.5.8. Electrically Controlled AMX Release from the Scaffolds

193 In the 'electrically controlled drug delivery' step, an OTA-CFA-based changeable pulse generator is utilized to observe the electric effect on AMX release at 50 Hz frequency value. 194 This circuit contains the square waveform generator, operational transconductional amplifier 195 196 (OTA), and current-feedback amplifier (CFA). The details of the circuit are given in a previous article carried out by Gunduz et al [10]. After the system was set up, nearly 5 mg of all scaffolds 197 were weighed and placed on the Eppendorf tubes with PBS (pH 7.4). The Ag/Pt electrode was 198 used to transfer the electricity to the PBS (1 mL) in the eppendorf tube. The experiment was 199 carried out at 50 Hz frequency and 10 V conditions. The electricity was applied to the scaffolds 200

for different time intervals. After the application of an electric field, the PBS was taken from
the Eppendorf tubes and absorbance values were detected at a wavelength of 230 nm.

203 2.5.9. Swelling and Degradation Properties of the Scaffolds

In the swelling test, all experimental groups were placed in 1 ml phosphate buffer saline (PBS) with pH 7.4. The scaffolds were held in a thermal shaker (BIOSAN TS-100) at 37 °C with 300 rpm. The initial weights (W₀) and the wet weights (W_w) of the scaffolds were measured daily. The swelling rate (SR) was measured with equation 2.

208
$$SR = \frac{W_W - W_0}{W_0} \cdot 100$$
 (2)

In the degradation test, the same procedure was used with swelling test. However after the incubation, he scaffolds were removed from PBS medium and dried in an incubator at 37 °C for 24 hours and the dried form weighed (W_t). The degradation rate (DR) was calculated by using equation 3.

213

$$DR = \frac{W_0 - W_t}{W_0} \cdot 100$$
 (3)

214 **3. Results and Discussions**

To investigate the interaction of chemical and molecular structure in produced CHT scaffolds, 215 FT-IR analysis was carried out on the four groups. These scaffolds that were containing 216 217 different concentrations of BFO, present the following specific vibrations: the characteristic absorption bands at 1565 cm⁻¹, 1375 cm⁻¹ 852 cm⁻¹, which are associated with familiar 218 219 vibrations for C=CH, N-H and saccharide [14]. The distinctive peak is in the absorption band at 815 cm⁻¹ in the spectrum for all experimental groups. The glycosidic bond is the strongest 220 peak in the entire spectrum (Figure 1 e). The characteristic bands of drug loaded BFO were 221 observed with a C=O vibration peak at 1295 cm⁻¹. A band, corresponding to the vibration of 222 N-N stretching was found at 1625 cm⁻¹, C=O stretching at 1037 cm⁻¹ (Figure 1 (b, c)). For 223 pure CHT, related peaks were found at 3283 cm⁻¹ representing the N-H stretching, C-H 224 vibration at 2869 cm⁻¹, and primary amide C=O stretching at 1589 cm⁻¹ (Figure 1 d) [15]. For 225

chitosan and bismuth ferrite combination groups, the absorption bands were observed at ~ 1577 cm⁻¹, 1375 cm⁻¹, 1022 cm⁻¹, and 863 cm⁻¹. These results indicate that molecular bonds of the pure CHT and AMX-loaded BFO are found in combinations.



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Figure 1. FTIR spectrums of the BFO (a), 6% CHT (b), 6% CHT/0.025% BFO (c), 6%
CHT/0.05% BFO (d), and 6% CHT/0.075% BFO (e).

Porosity is important for controlling the rate of drug release, while surface roughness affects the adhesion of cells and proteins. The viscosity of the 3D printing ink has a major effect on the final 3D printed structure. Low viscosity can cause the chitosan ink to flow too quickly and create a rough surface finish or drooping layers. On the other hand, a viscosity that is too high can cause clogging of the nozzle and disruption to the printing process. Chitosan with high molecular weight chitosan may result in greater strength and stiffness of the printed product.
The concentration of the nanoparticles in the ink may also affect the resolution and accuracy of
the printed product. Furthermore, the BFO nanoparticles can increase the porosity of the 3D
printed part, which can be beneficial for applications such as drug delivery or tissue
engineering.

Knowing that BFO is a ferroelectric material with a high piezoelectric response it can be used 242 to generate an electric field in the composite. This electric field can help to promote cell 243 attachment and spreading, as well as the supporting the adhesion of cells to the biopolymer. It 244 could also alter the behavior of the cells, by inducing changes in the expression of certain genes 245 246 and proteins [16]. In addition, the electric field may also affect the properties of the biopolymer, such as its mechanical strength, chemical stability, and biocompatibility. Thus, adding BFO to 247 248 a biopolymer composite can significantly impact cell attachment and behavior of the final composite. 249

Figure 2 (a, b) represents the TEM images of the BFO particles. In the TEM images, uniformly formed nanoparticles can be seen. The morphologies of the particles show that they are agglomerated with an almost spherical shape. This agglomeration can be attributed to the coprecipitation method, which produces particles of very small size [17].

Figure 2 (c-f) highlights the morphology of the fabricated scaffolds at two different magnifications (100X and 200X), with all structures characterized by a well-defined geometry and structure, indicating the control and fidelity of the scaffold fabrication process.



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Figure 2. The TEM images of the BFO particles (a, b), the SEM images of the 3Dprinted scaffolds, 6% CHT (c), 6% CHT/0.025% BFO (d), 6% CHT/0.05% BFO
(e), and 6% CHT/0.075% BFO (f).

The DSC curves of BFO (loaded with amoxicillin) and the 3D-printed scaffolds are presented 261 in Figure 3. It was observed that a minor endothermic peak as a result of dehydration of AMX 262 occurs at ~ 100°C. A minor broad endothermic peak, due to AMX fusion degradation at 190-263 ~222.3°C was also observed [18]. Figure 3 shows that a steep exothermal peak occurs at ~230 264 ^oC, which is attributed to a mass loss of the BFO due to its decomposition to Fe(OH)₃ and 265 Bi(OH)₃ metastable states [12]. These metastable states of Bi(OH)₃ and Fe(OH)₃ are 266 subsequently transformed to stable Bi₂O₃ and Fe₂O₃ phases, respectively [12]. The stable phases 267 (i.e. Bi₂O₃, Fe₂O₃ phases) further decompose at ~570 °C, as highlighted by the weak peak 268 observed. The additional phase transition of BFO at curie temperature (830 C) was not 269

observed due to the temperature limit (600 °C) of the equipment employed in the present study 270 271 [12]. The DSC of the 6% CHT scaffold also highlighted some characteristic endothermic peaks at ~50 °C, ~92 °C and ~150 °C which may be due to the evaporation of the residual solvent 272 (i.e. acetic acid) employed during scaffold preparation. These peaks are also present in the DSC 273 curves of 6% CHT/0.025% BFO, 6% CHT/0.05% BFO, and 6% CHT/0.075% BFO, albeit 274 diminished, as the BFO concentration becomes progressively higher. An exothermic peak was 275 observed at ~270 ° C, which is associated with the depolymerization, dehydration of the 276 saccharide ring, and deacetylated and acetylated chitosan units decomposition [19]. Due to this 277 degradation, the melting temperature was not observed. Indeed, it was reported that the 278 279 amorphous region in the chitosan results in the dispersion of the energy points [19]. As expected, other chitosan-based scaffolds also presented similar decomposition peaks, which 280 were observed to be less intense as the concentration of the BFO was progressively increased. 281







Figure 3. DSC curves of the synthesized BFO and 3D-printed scaffolds.

The tensile strength of a 3D-printed chitosan scaffold is an important factor for determining its biocompatibility and suitability for tissue engineering applications. Strain at break and tensile strength are two important parameters used to evaluate the mechanical properties of 3D-printed natural polymer scaffolds. The strain at break is a measure of the scaffold's ability to withstand an applied load before it fails. It measures the degree of deformation a scaffold can withstand before it permanently deforms or breaks. The tensile strength is a measure of the amount of force required to break the scaffold.

The tensile strength of 3D printed chitosan scaffold is largely determined by the type of printing 291 process used, the concentration of chitosan in the 3D printing medium, and the type of solvent 292 293 and crosslinker. Additionally, the use of a higher concentration of chitosan in the 3D printing medium can increase tensile strength. The tensile strength of 3D printed chitosan scaffold can 294 also be improved through the addition of reinforcing agents such as carbon nanotubes and 295 graphene [20-22]. These materials can be used to increase the tensile strength of the scaffold 296 297 by increasing the intermolecular interactions between the chitosan molecules and reinforcing 298 agents. In this study, by the addition of 0.025% of BFO to the scaffold formulation, the tensile 299 strength and strain at break of the scaffolds increased. We observed about 1 MPa increase in tensile strength and about 7% in the strain at break, however, further increase of BFO 300 (>0.025%) had a negative impact on the tested parameters (Table 1 and Figure 4). Therefore a 301 balanced concentration of BFO could improve the mechanical properties of the scaffold. 302

Table 1. Tensile strength and strain values of the dry 3D printed scaffolds

Scaffolds	Tensile strength (MPa)	Strain at break (%)
6% CHT	4.01 ± 1.04	5.34 ± 0.82
6% CHT/0.025% BFO	4.97 ± 0.34	12.09 ± 4.73
6% CHT/0.05% BFO	4.61 ± 1.38	7.59 ± 1.73
6% CHT/0.075% BFO	3.08 ± 0.77	10.09 ± 0.19





Figure 4. The stress-strain curve of the 3D-printed scaffolds.

Figure 5 shows the XRD patterns of scaffolds for the assessment of the crystalline phases 306 present. To this regard, the XRD patterns of the scaffolds, based on BFO, 6% CHT, 6% 307 308 CHT/0.025% BFO, 6% CHT/0.05% BFO, and 6% CHT/0.075% BFO and designated as Figure 5 (a),(b), (c), (d) and (e) respectively were presented. Figure 5 shows that the major diffraction 309 310 peaks at 20 angles of 39.41°, 45.68°, 65.9° and 76° were observed in the XRD of BFO (Figure 5 a). These peaks are consistent with some of the major peaks of the XRD pattern of single-311 phase BFO with a distorted perovskite structure [23]. However, other peaks at 20 angles of 312 22.34°, 27.6°, 31.68°, 32°, 51.24°, and 57.1° that characterize crystalline BFO nanoparticles 313 314 according to (JCPDS Card No. 86-1518) were absent [23]. This suggests the reduced crystallinity of the BFO prepared in the present study. This observation is expected since the 315

'as prepared' BFO sample (i.e. without further treatment) has been reported to present a mainly 316 317 amorphous nature [24]. This outcome may be due to the low temperature imposed during the preparation approach and the absence of the calcification step. Notably, the low temperature 318 imposed in the BFO preparation approach may explain the absence of impurity peaks. This is 319 because, the application of low temperatures (i.e. < 450 °C [25]) may reduce the risk of 320 secondary impurity peaks such as Bi₃₆Fe₂O₅₇ and Bi₃Fe₄O₉ typically detected at 20=29.39°, 321 25.69° and 34.12° [25]. Crucially, the absence of the characteristic peaks of amoxicillin 322 reported to typically occur at 20 angles of 18.1°, 19.5°, 23.1°, 26.4° and 28.3° [26] in the XRD 323 pattern presented in Figure 5 (a) may be due to its low concentration. Indeed, the literature 324 325 suggests that if the concentration of BFO is higher than the concentration of amoxicillin, the XRD patterns due to BFO may be sufficient to dispel X-rays, leading to a weaker signal overall 326 [27]. Amoxicillin drug presence will therefore be demonstrated using additional tests (i.e. drug 327 328 release kinetics etc.) as discussed in subsequent sections. Figure 5 also shows that the 6 % CHT sample presents peaks in 2θ at 10.5° and 19.8° , which are associated with the (020) and (100) 329 crystallographic planes, respectively. These peaks are indicative of the typical chitosan 330 structure [28]. Notably, in the XRDs for the scaffolds of Figure 5 (b), (c), (d), and (e), the 331 intensity of the peaks in 20 at 10.5° and 19.8° is slightly diminished when compared to the XRD 332 333 of pure chitosan reported in the literature [29]. The reduced intensity of the peaks may be due to the application of acetic acid in the preparation of the 6% CHT solution since the acetic acid 334 has the potential of breaking down the crystal regions present in chitosan when it is dissolved 335 336 [30].





Figure 5. XRD peaks of the synthesized BFO (a), 6% CHT (b), 6% CHT/0.025% BFO (c),
 6% CHT/0.05% BFO (d), and 6% CHT/0.075% BFO (e) scaffolds.

Figure 6 shows the quantitative analysis of cell viability in the presence of the different 340 341 scaffolds based on 6% CHT, 6% CHT/0.025% BFO, 6% CHT/0.05% BFO, and 6% CHT/0.075% BFO, using the MTT assay. It was observed that, after 24 h of culturing the cell 342 proliferation in all scaffolds was comparable. Notably for 6% CHT and 6% CHT/0.025% 343 scaffolds, the cell proliferation at 96 h was less than the cell proliferation at 24 h. This 344 observation may be indicative of the requirement for the cell to attain the necessary stationary 345 phase due to the increased surface area available for proliferation as the BFO content increases 346 [31]. Figure 6 also shows a positive correlation between the cell proliferation and the BFO 347 content after 96 h and 168 h of cultivation. This enhanced cell proliferation is reinforced in the 348 SEMs (Figure 7) and is due to the increase in the overall porosity of the scaffolds by cause of 349 higher concentrations of BFO nanoparticles. Indeed, the poor cell proliferation in the CHT 350 scaffold could be because of the low porosity which can hinder cell anchorage and adhesion, 351

even leading to cell death [32]. The enhanced cell proliferation of the scaffold with increasing BFO content is observed in Figure 7 with the increase in the concentration of BFO nanoparticles contributing to the roughness of the scaffold surface. The increased surface roughness enables the cells to attach to the matrix with the cells subsequently dividing to form non-uniform cell clumps. Figure 8 shows the fluorescence images of the scaffolds after 1, 4, and 7 days of incubation and results showed that the cell distribution was higher for all scaffolds than the cell distribution obtained on 1st day.



Figure 6. MTT graph of the 3D-printed scaffolds after 24, 96, and 168 hours ofculture period with fibroblast cells.





Figure 7. SEM images of the 3D-printed scaffolds after 7 days of incubation.





Figure 8. Fluorescence images of the scaffolds after 1, 4, and 7 days of culture period. 365 The results of our drug release studies indicate that the addition of BFO can significantly 366 enhance the release rate of the drug from the chitosan composite (Figure 9a). This is attributed 367 to the presence of nanoparticles, which create a large surface area for drug adsorption and 368 release. Additionally, the magnetic properties of BFO can be used to control the drug release 369 rate and direction, allowing the drug to be released in a controlled manner. The incorporation 370 371 of BFO into the chitosan composite increased the AMX drug release rate by reducing the particle size and increasing the porosity of the composite. The smaller particle size of BFO 372 allows for greater drug diffusion through the composite, resulting in an increased release rate. 373 374 Additionally, the enhanced porosity of the composite due to the incorporation of BFO expands the surface area for drug diffusion and thus increases the drug release rate. In addition, BFO 375 can also modulate the release of AMX by its ferroelectric properties. The ferroelectric 376 properties of BFO allow for the application of an electric field which can be used to control the 377 release rate of AMX. The electric field affects the orientation of the dipoles in the BFO, thus 378 379 changing the porosity of the composite and resulting in increased or decreased release of the drug (Figure 9b). According to the results, it can be said that by adjusting the applied current's 380 characteristics, the delivery can be customized to the needs of the patient. Electrically triggered 381

drug release also has the potential to get around some of the drawbacks of traditional drugdelivery methods, such as low drug efficacy and possible adverse effects [33].



Figure 9. Drug release behaviors of the AMX from the scaffolds, without electric field (a),under electric field (b).

384

The swelling and degradation profiles of the scaffolds were given in Figure 10 (a, b). To protect 387 the wound from infections, an ideal wound dressing must maintain a moist environment while 388 absorbing wound fluids [34]. The swelling rates of the scaffolds were showed in Figure 10a. 389 The all 3D-printed scaffolds were exhibit a swelling profile up to the 4th day. The 6% 390 CHT/0.025% BFO and 6% CHT/0.075% BFO scaffolds exhibited similar swelling rates and it 391 was lower than the swelling rate value of 6% CHT scaffold. The reason for the high swelling 392 rate of chitosan may be its porous structure [12]. The 3D-printed scaffolds were started to 393 degrade on the 6th day. Saatcioglu et al. fabricated Chitosan/Osage orange extract scaffolds and 394 reported that the highest swelling ratio was belonged to the only 6% CHT scaffold [12]. The 395 3D-printed scaffolds were exposed to PBS and weight loss over time was recorded. The 396 degradation rates of 6% CHT, 6% CHT/0.025% BFO, 6% CHT/0.05% BFO, and 6% 397 398 CHT/0.075% BFO scaffolds were showed in Figure 10b. For the first 48 h, the scaffolds loss nearly 35% of their weights. According to the results, all the scaffolds were exhibited 399 proportional degradation profile. 400





Figure 10. Swelling and degradation profiles of the 3D-printed scaffolds.

403 **4.** Conclusions

404 This study demonstrated the feasibility of using 3D printing technology to fabricate a chitosanbased wound dressing with the addition of bismuth ferrite (BFO) nanoparticles. BFO loaded 405 chitosan based scaffolds were characterized physicochemically and results showed that BFO 406 nanoparticles were successfully loaded into the chitosan scaffolds. SEM imaging showed that 407 the BFO nanoparticles increased the porosity of the 3D printed scaffolds that improves drug 408 409 release profile and good for cell attachment with high biocompability. The drug release rate of 410 amoxicillin from the composite was significantly enhanced with the addition of BFO, which can be attributed to the small particle size and increased porosity of the composite. Additionally, 411 412 the incorporation of BFO increased the mechanical strength and strain at break of the the 6% CHT scaffold, which is important for tissue engineering applications. The results of fibroblast 413 culturing showed that the cells successfully adhered onto scaffolds and maximum cell viability 414 415 was observed for 6% CHT/0.075% BFO scaffolds. Finally, the ferroelectric properties of BFO can be used to modulate the release of AMX by applying an electric field (10V, 50 Hz),, thus 416 417 providing a controlled release system, suggesting that AMX release could be controlled with the application of electricity. This study demonstrates the potential of using 3D-printed chitosan 418 scaffolds with BFO nanoparticles for controlled drug delivery in wound dressings. The printed 419

chitosan based scaffolds that improved as electrically conductive, can be used in triggered drug
relase applications. In this manner, controlled drug release enhanses the wound healing to a
visible extent.

423 Data availability

424 The raw data will be made available upon request.

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