



## Improving the atmospheric plasma deposition of crystalline inorganic coatings

A. Remy<sup>a</sup>, M. Serigne Fall<sup>a</sup>, T. Segato<sup>b</sup>, S. Godet<sup>b</sup>, M.P. Delplancke-Ogletree<sup>b</sup>, P. Panini<sup>c</sup>, Y. Geerts<sup>c</sup>, F. Reniers<sup>a,\*</sup>

<sup>a</sup> Université libre de Bruxelles, Faculty of Sciences, Chemistry of Surfaces, Interfaces and Nanomaterials – ChemSIN, cp 255, Avenue F.D. Roosevelt, 50 – B-, 1050 Brussels, Belgium

<sup>b</sup> Université Libre de Bruxelles, 4MAT, cp 165/63, Av. F.D. Roosevelt, 50 – B-, 1050 Brussels, Belgium

<sup>c</sup> Université Libre de Bruxelles, Faculty of Sciences, Laboratoire de Chimie des Polymères, cp 206/01, 50-B-, 1050 Brussels, Belgium

### ABSTRACT

The deposition of good quality crystalline inorganic coatings by atmospheric pressure dielectric barrier discharge remains a challenge. Thanks to an original coupling of a substrate heating device based on an inductive current loop and located under the dielectric and an atmospheric pressure dielectric barrier discharge, we show that one can deposit in one step crystalline vanadium oxide and titanium oxide, with grain sizes bigger than those achieved by post-deposition annealing.

### 1. Introduction

The deposition of thin films using physical vapour deposition (PVD) or plasma-enhanced chemical vapour deposition (PECVD) using low pressure plasma systems has been the subject of thousands of papers these last 40 years. Techniques such as DC-sputtering, magnetron sputtering [1], radiofrequency (RF) sputtering [2–4] or more recently HiPIMS [5] have been developed and optimized thanks to hundreds of researchers. Metallic, organic and inorganic coatings can now be deposited with an extreme reproducibility, at high speed, with controlled crystallinity. Industrial vacuum coater lines are implemented throughout all the world. The evolution of the concepts in thin film sputter deposition can be found in [6]. In this review, it is shown that the deposition of the right coating not only required the right chemistry, but also the right structure, a controlled number of defects and the right crystallinity. Because of the crucial importance of these structural parameters, research has been focused on low pressure techniques and/or techniques such as chemical vapour deposition that may use high temperature. The key concept of getting crystalline coatings and structure-controlled coatings is the energy available at the surface. This energy may be brought by the incoming particles themselves, by further resputtering of the surface, or from heating of the substrate. Appropriate surface preparation is also often required to achieve the best coating. A side parameter is also the deposition time, as a conventional approach tells us that one needs to operate at low deposition rates to obtain the best coatings. Although the contribution of our group was minor in that domain, we also could deposit epitaxial films of Ag, Pd,

and AgPd alloys, Cu, Rh, Pd, CuPd and CuRh alloys [7] as well as crystalline carbide and nitride films (MoC, WC, MoN, WN, CrC [8,9]). Classically, most of such coatings that provide a significant added value to the material are deposited under vacuum, as it offers an excellent control on the remaining gas impurities, it allows tuning the energy of the particles arriving on the substrate thanks to their high mean free path, and it allows complex chemistry (oxides, carbides, nitrides, alloys, ...). However, amongst main constraints are the complexity of industrial vacuum coater lines, and very often a limited deposition rate. Although these remarks must be counterbalanced by the many improvement of all the above-mentioned techniques, they are often in the back of the mind of the researchers and the coatings manufacturers. Other approaches were therefore developed, such as chemical vapour deposition (CVD), but it necessitates usually high temperatures, or sol-gel deposition, but it requires most often a high temperature post-annealing treatment to remove the solvents and to give its final texture to the coating.

Atmospheric plasmas have been used for a long time for ozone synthesis (the Siemens process dates from 1857 [10]) and for surface activation. Their main advantage is their ability to be run at atmospheric pressure, avoiding therefore the need of vacuum systems (chambers, pumps, transfer locks...). For this reason, ultrahigh speed (up to 500 m/min) surface treatment can be achieved for surface activation of materials, or for instance, for the surface cleaning of metals [11]. However, the main advantage of atmospheric plasma is also their main drawback when it comes to deposition of coatings: because they are run at atmospheric pressure, without pumping, the gas is not well

\* Corresponding author.

E-mail address: [freniers@ulb.ac.be](mailto:freniers@ulb.ac.be) (F. Reniers).

<https://doi.org/10.1016/j.tsf.2019.137437>

Received 1 May 2019; Received in revised form 19 July 2019; Accepted 19 July 2019

Available online 20 July 2019

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controlled, introducing impurities in the coatings, and the mean free path is very small, leading to incoming particles having an extremely low energy. For this reason, the first depositions were dedicated to organic coatings, to synthesize random “plasma polymers” and to the deposition of amorphous inorganic coatings in their oxide form, like SiO<sub>x</sub>, acting as barrier layers for oxygen, water or corrosion [12].

Another drawback is the presence of residual air in chambers that, for a long time, prevent researchers to deposit coatings that could be easily oxidised (like Si).

The atmospheric plasma deposition of organic coatings (often named “plasma polymers”) has been the subject of hundreds of papers and many reviews can be found in the literature [13–16]. People can deposit PVC-like polymers [17], polytetrafluoroethylene-like [18], acrylates [19], biocompatible polyethylene glycol [20], superhydrophobic [21], hydrophilic coatings [22], silane-based [23], polystyrene [24].

When it comes to crystalline inorganic coatings, for years, the main option was to perform annealing on the quasi-amorphous deposited films. Another option is the resistive heating of the substrate during deposition. This option is however often hard to realize in real experimental conditions, as most of the atmospheric plasma deposition is done using a high frequency (in the 1–100 kHz range) dielectric barrier discharge. Amongst the main problems are electrical interferences between the heating circuit and the plasma circuit, and the difficulty to heat a substrate placed on a dielectric material. Nevertheless, a few studies report successful use of a resistive heating system to deposit, for instance, TiO<sub>2</sub> in anatase phase [25].

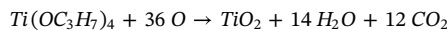
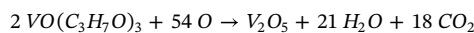
We propose in this paper an original approach for heating the substrate, new for atmospheric plasma discharge, based on a secondary inductive electrical circuit placed at one of the two electrodes of a DBD, under the dielectric. This system allows, as for some of the low pressure deposition systems, to deposit crystalline inorganic coatings. Vanadium oxide and titanium oxide are selected as examples in this paper to show the feasibility of the process. They are chosen for their wide applications, and for their various crystalline forms and oxidation states. Vanadium oxides can be used for infrared sensors [26], as catalysts [27], as thermochromic or electrochromic devices [28] and as cathode for Li-ion batteries [29]. Vanadium has also 5 different oxidation states. Titanium oxide is well known as photocatalyst, where it has been shown that, in most conditions, the anatase form or a mix of rutile and anatase are the most active ones [30].

## 2. Experimental

The precursors used for this study are vanadium oxytriisopropoxide (VOTP) from Alfa Aesar (product # 89798 CAS # 5588-84-1) and titanium tetraisopropoxide (TTIP), from Sigma-Aldrich (Product #205273 CAS#546-68-9). They are chosen for their limited toxicity and hazardous properties and for their high vapour pressure. The precursors are introduced inside the plasma chamber by bubbling argon into the heated liquid precursors. Argon (Air Liquide P0021L50S2A001) is used as the carrier gas for the precursors, and as the main plasma gas. Oxygen (Air Liquide P0361L50R2A001) is used as secondary reactive gas. The substrates used for this study are Si wafer (N doped (001) oriented from Pi-Kem), Au (coated on glass), and Al 2024 alloy, and are selected for their appropriate properties for the characterization techniques. Before deposition, substrates were cleaned with methanol and isooctane to avoid contamination. Deposition is realized in the home made DBD chamber whose schematic is presented in Fig. 1. The power generator is an AFS G10S-V instrument operating at 19 kHz in our conditions. The injected power was varied from 0 to 80 W in this study.

The main parameters used for the deposition of coatings are summarized in Table 1.

Although the chemical mechanisms are complex, the two chemical reactions can be summarized as:



where the atomic oxygen originates from the dissociation of O<sub>2</sub> in the plasma.

### 2.1. Heating device [31]

Induction heating is a long-time known way to heat metals by the magnetic induction of an alternating current (Eddy current) into a conductor. The principle and details of the induction heating technique is very well understood and described for instance in [32].

The device proposed here is not intended to heat the substrate itself directly (although it is the case if the substrate is a conducting material). Instead, a heating susceptor is placed under the substrate. The susceptor is made of thin sheet of a conducting material, preferably with a high melting point and a high Curie point.

The heating device consists in an inductive coil rounding a ferrite block placed under the bottom electrode and a susceptor placed between the bottom dielectric and the substrate. As the bottom electrode is above the inductive coil and under the dielectric, its geometry contains holes to allow the magnetic loops to reach the susceptor. A schematic of the heating device is presented in Fig. 2.

The electrode used (called hollow electrode) is a disk made of a good conductor (Aluminum, 50 mm of diameter) that has a slit from the side to the center to avoid the apparition of Eddy current in the electrode. As the coil is placed underneath the center of the electrode, and has a smaller diameter than the electrode itself, the center of the electrode is a hole of the diameter of the coil, also to avoid heating. The susceptor is placed above the hole in such a way that magnetic loops are perpendicular to it. The thickness of the susceptor is an important parameter since it will affect its resistance through the skin effect and as described in Fig. 2.

The heating device build on this principle uses an alternating current of 17,5 V and 4 A at a frequency between 20 and 80 kHz passing through a Litz wire cable wrapped six time around a ferrite core of 20 mm and constituting the heating coil. The susceptor is made of a copper foil of 0.1 mm thick and 25 mm of diameter this configuration allows to reach 573 K in 1 min. The temperature is measured on top of the substrate without the plasma and using a thermocouple K.

The deposited coatings are characterized using X-ray diffraction (Rigaku Ultima IV diffractometer for V<sub>2</sub>O<sub>5</sub> coatings and a D8 Advance Eco Bruker diffractometer with Cu Kα (λ = 1.5418 Å) and 1,5° of grazing angle for TiO<sub>2</sub> coatings), X-ray photoelectron spectroscopy (Physical Electronics, PHI 5600 spectrometer using the Mg anode operating at 200 W), and Fourier transform infrared spectroscopy (Nicolet 5700 spectrometer). Commercially available V<sub>2</sub>O<sub>5</sub> (J.T.Baker CAS#1314-62-1), VO<sub>2</sub> (Sigma-Aldrich CAS#12036-21-4) and TiO<sub>2</sub> powders (Sigma-Aldrich Product#232033) are used as references.

## 3. Results

### 3.1. Vanadium oxide

Using PECVD it has been shown that one could deposit crystalline V<sub>2</sub>O<sub>5</sub> at lower temperatures than those used for conventional CVD. Barreca et al. [33] showed that VO(hfa)<sub>2</sub>·H<sub>2</sub>O in a low pressure PECVD process can deposit V<sub>2</sub>O<sub>5</sub> in highly oriented orthorhombic phase at only 423 K, Musschoot et al. got the same temperature for PE-ALD of O<sub>2</sub> and vanadium triisopropoxide oxide [34]. However, such studies were conducted at low pressure. For CVD the process usually needs a post-deposition annealing to obtain a crystalline phase or a deposition at high temperature. Piccirillo et al. [35] used V(acac)<sub>3</sub> and VO(acac)<sub>2</sub> to obtain crystalline VO<sub>x</sub> at atmospheric pressure and 773 K, Field et al. [36] used VOCl<sub>3</sub> and VCl<sub>4</sub> in an APCVD reactor at 733 K to obtain V<sub>2</sub>O<sub>5</sub>, Manning et al. [37] deposited VO<sub>x</sub> with VCl<sub>4</sub> by APCVD process at

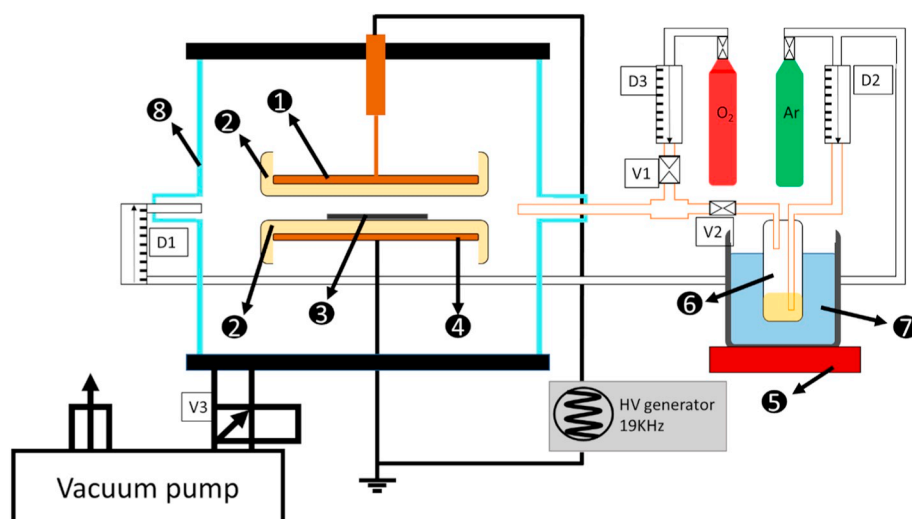


Fig. 1. Schematic of the deposition setup. 1) High voltage electrode; 2) Dielectric; 3) Substrate; 4) Ground electrode; 5) Heating plate; 6) Bubbler; 7) Thermostated water bath; 8) Closed chamber; V1) Dioxygen valve, V2) Precursor valve, V3) Atmospheric pressure equalization valve; D1) Argon main plasma gas flowmeter; D2) Argon carrier flowmeter; D3) Dioxygen flowmeter.

temperatures between 733 K and 833 K, Mathur et al. [38] used low-pressure CVD with VOTP to synthesize  $\text{VO}_x$  by varying the substrate temperature between 673 K and 973 K.

In this study, starting from VOTP as precursor, to reach vanadium oxide, carbon and hydrogen must be removed. A pure Argon discharge leads to the deposition of a coating still contaminated with carbon and the XPS spectrum of the Vanadium peaks (V 2p 3/2 and 1/2) (Fig. 3) reveals the presence of vanadium in the +5 but also in the +4 oxidation state. Their respective binding energies for the V2p 3/2 are 517.2 eV and 515.8 eV. This indicates that vanadium, originally in the +5 state in the precursor is partly reduced by the plasma. Indeed, the V5+ peak represents 60% of the Vanadium peak area when the coating is deposited at 50 W, but only 44% when it is synthesized at 60 W. The shoulder on the high energy side of the O1s peak can be attributed to a carbon-oxygen component coming from the carbon contamination (between 40% and 43% given by the full survey of the coatings between 50 W and 60 W) of the coating due to the absence of oxygen in the gas flow.

Increasing the oxygen pressure in the discharge leads to a decrease of the carbon content, and to a decrease of the V + 4 state conjugated with an increase of the V + 5 state. This is clearly visible on the evolution of the XPS spectra (Fig. 4), where the V 2p3/2 peaks shifts towards higher binding energies with increasing %O<sub>2</sub> in the discharge. The high energy shoulder centered at 532,5 eV of the O 1s peak on the 3% oxygen spectrum is due to the presence of the underneath native silicon oxide layer of the Si substrate.

### 3.2. Deposition of $\text{V}_2\text{O}_5$ in an argon/oxygen discharge, on an inductively heated substrate

Fig. 5 shows the IR spectra of the coatings deposited on substrates heated at various temperatures. At 373 K, the CH and OH bands are clearly identified, as well as the two main bands of V=O and O-V-O [39] at 1005 and 810  $\text{cm}^{-1}$  respectively [40]. The presence of CH bands at low temperatures, even with 5% O<sub>2</sub> in the reactor, indicates that the reaction is not complete in these conditions. At 473 K, only the V=O and O-V-O bands remain, whereas not C-H nor OH bands are detected anymore. A further increase in temperature leads to a sharpening of the

Table 1

Plasma deposition parameters used for the deposition of vanadium oxide and titanium oxide.

	Tot. flux (L/min)	O <sub>2</sub> (L/min)	Ar carrier (L/min)	Ar plasma (L/min)	Bubbler temperature (K)	Substrate	Substrate temperature (K)
V <sub>2</sub> O <sub>5</sub>	10	0-1	1	8-9	308-313	Si - Al - Au	273-673
TiO <sub>2</sub>	10	1	0.5-2	7-8.5	333	Si	673

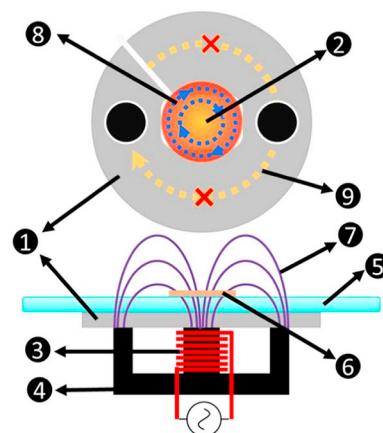
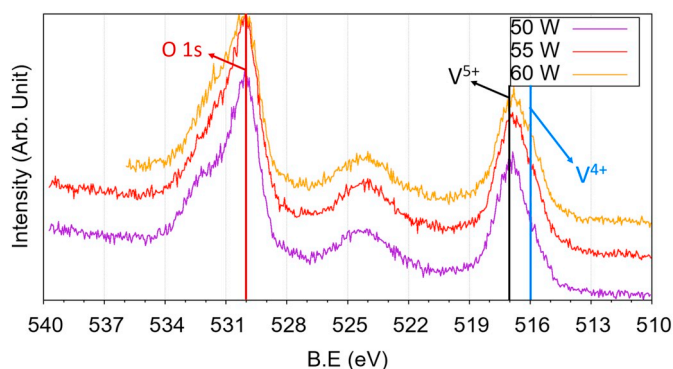


Fig. 2. configuration with hollow electrode. 1) Electrode; 2) Heated zone; 3) induction coil; 4) ferrite core; 5) Dielectric; 6) Susceptor; 7) Magnetic field lines; 8) induced Eddy current (arbitrary direction); 9) impossible current line.

V=O band and to a decrease in intensity of the V-O band. A shift of the V=O and V-O bands to higher wavenumbers is also observed, suggesting a higher crystallinity of the  $\text{V}_2\text{O}_5$  coating and, as suggested by Liedberg et al. [41], this behavior is the mark of a strong anisotropy of the coating, given a greater absorption of the V=O band oriented perpendicular to the surface of the substrate.

Fig. 6 shows a comparison of the XRD pattern of  $\text{V}_2\text{O}_5$  deposited on a gold substrate at 573 K and a coating deposited at room temperature and further annealed at 573 K.

From the global XRD diagram, one can already distinguish a better crystallization. Calculating the average size of the crystals from the Scherrer equation, gives values of 13 nm for the coatings obtained by post-annealing, and of 16 nm for the coatings deposited directly at 573 K. These values are however purely indicative, and overestimate for the annealed coating, as it presents very small XRD peaks (see Fig. 6). The average thickness of the coatings, as measured by SEM cross-sectioning, is 56 nm, for a 20 min deposition time. This gives a 2.8 nm/min average deposition rate.



**Fig. 3.** XPS O1s, V2p1/2 and V2p3/2 peaks of coatings deposited from VOTP in an argon discharge at different injected powers. An increase in power leads to an increase in the V + 4 component, indicating partial reduction of the vanadium, originally in the +5 state in the precursor. Conditions are 308 K VOTP, 1 L/min argon carrier, 10 L/min total flux and 20 min of deposition time on silicon wafer at 298 K.

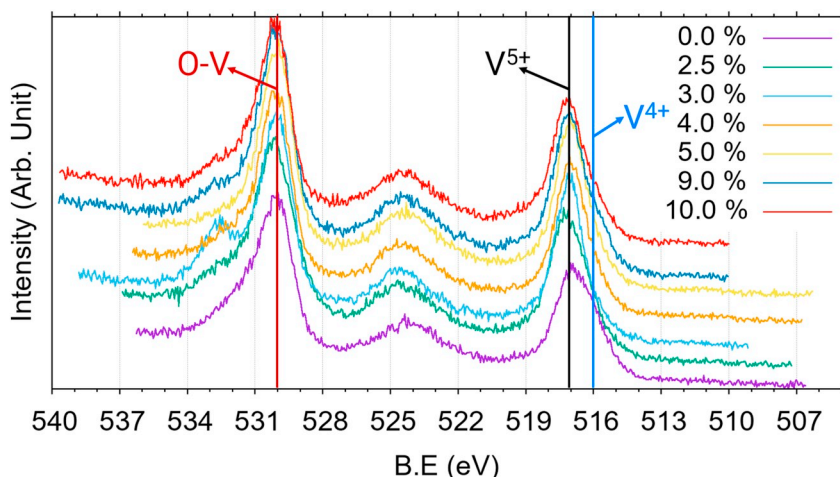
### 3.3. Deposition of TiO<sub>2</sub>

A few studies report de deposition of TiO<sub>2</sub> in the anatase form using atmospheric plasma techniques: [25,42,43]. They use conventional resistive devices to heat the substrate at 573 K [25], 673 K [42] or they use the heat generated by the plasma itself (around 463 K) to obtain a crystalline phase [43].

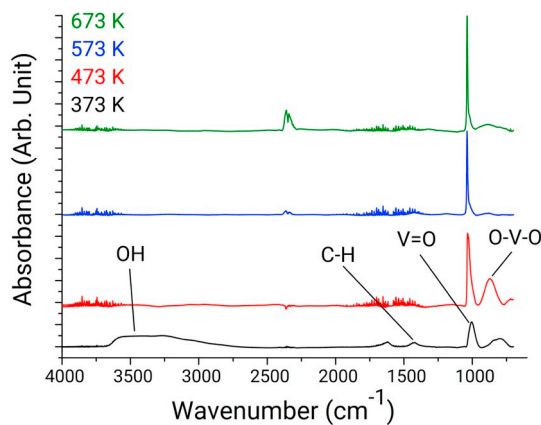
The deposition of TiO<sub>2</sub> films from TTIP proceed from the same rationale as for vanadium oxide. The TTIP must be fragmented inside the plasma, and the carbonaceous fragments are removed by oxidation, if oxygen is added in the discharge. The experimental procedure for the synthesis of TiO<sub>2</sub> using an atmospheric DBD, TTIP, Ar and oxygen has already been published, as well as the effect of the plasma parameters on the morphology, composition and catalytic activity of the films deposited. They will not be repeated here. Chen, using the same setup, obtained amorphous TiO<sub>2</sub> films, onto room temperature substrates [44,45]. After annealing 2 h at 673 K, small crystals of anatase were formed, and exhibit a photocatalytic activity. This is however a two-step process that leads, as shown for vanadium oxide, to a lower degree of crystallization than direct heating of the substrate.

Fig. 7 a and b show the XRD patterns of TiO<sub>2</sub> coatings deposited on Si and Al at 673 K. It reveals clearly the diffraction peaks of Anatase.

Chen et al. [44,45], on the same setup, with annealing at 673 K but

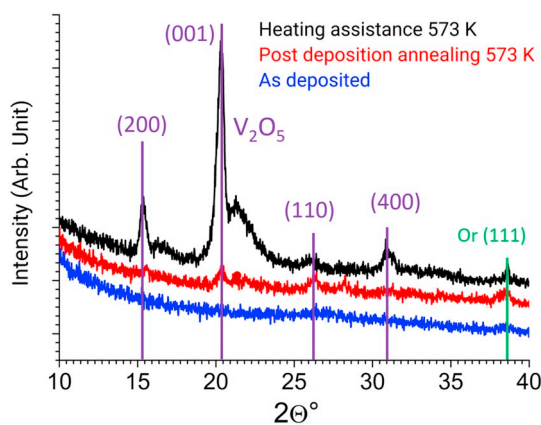


**Fig. 4.** XPS O1s, V2p1/2 and V2p3/2 peaks of coatings deposited from VOTP in an argon/oxygen discharge at different oxygen concentrations. An increase in oxygen leads to a decrease in the V + 4 component. Conditions are 310 K VOTP, 1 L/min argon carrier, 10 L/min total gas flux, O<sub>2</sub> from 0,25 L/min to 1 L/min and 20 min of deposition time on silicon wafer at 298 K.



**Fig. 5.** IR spectra of coatings deposited at different substrate temperatures. The deposition conditions are 30 W, 5% of O<sub>2</sub>, VOTP 310 K, 1 L/min of Argon carrier gas, 10 L/min total gas flow, 20 min of deposition time on aluminum 2024 substrate.

A major advantage of in situ, during deposition, heating is that it leads to a better crystallization than post-treatment annealing.



**Fig. 6.** Deposition of V<sub>2</sub>O<sub>5</sub> by atmospheric plasma onto an Au substrate at 10% oxygen in the gas phase, 50 W of power and 310 K of VOTP. Gas flux are 1 L/min of carrier gas, 10 L/min of total flux and 20 min of deposition time on gold substrate.

without heating the substrate during deposition, determined an average crystal size of 7.9 nm (based on the (101) diffraction peak of TiO<sub>2</sub>). For coatings deposited onto the inductively heated substrate, the average

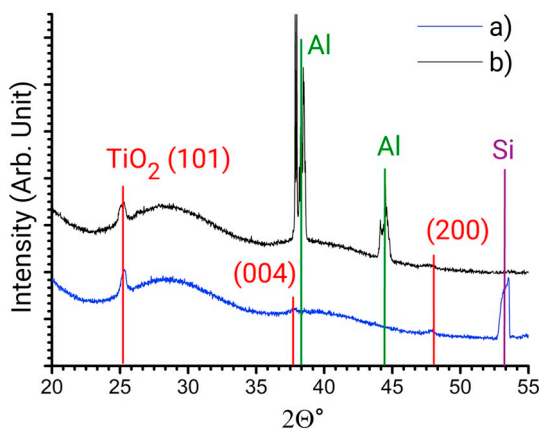


Fig. 7. a: XRD diagrams of TiO<sub>2</sub> films deposited onto silicon with the substrate heated at 673 K. Deposition conditions: 0,5 L/min argon carrier, 10% O<sub>2</sub>, 10 L/min total flux, 30 W of power and 20 min of deposition. b: XRD diagrams of TiO<sub>2</sub> films deposited onto aluminum, with the substrate heated at 673 K. Deposition conditions: 2 L/min argon carrier, 10% O<sub>2</sub>, 10 L/min total flux, 30 W of power and 20 min of deposition.

crystal size is 22.4 nm.

#### 4. Conclusions

Deposition of crystalline coatings using cold atmospheric pressure plasma, once a real challenge due to technological constraints, is facilitated by an inductive heating device of the substrate conveniently located under the dielectric and the bottom electrode. This original setup avoids electrical interferences with the high frequency plasma circuit. It allows fast heating of the substrate, located on top of a dielectric. Crystalline vanadium oxide (V<sub>2</sub>O<sub>5</sub>) and titanium oxide, anatase (TiO<sub>2</sub>) can now easily be grown using an atmospheric DBD, starting from volatile organometallic precursors.

Although the quality of the deposited coatings still remain way below those deposited using low pressure PVD or PECVD techniques, one should remember that the latter ones are much more matured, and where developed since many decades, contrary to the much younger atmospheric pressure thin film deposition.

#### Acknowledgements

This work is funded by the EoS (Excellence of Science, Belgian National Research Fund) project “Nitroplasm”, and by the Walloon Region (project Amorpho).

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