

Evaluating Mechanical Properties of Polymers at the Nanoscale Level via Atomic Force Microscopy–Infrared Spectroscopy

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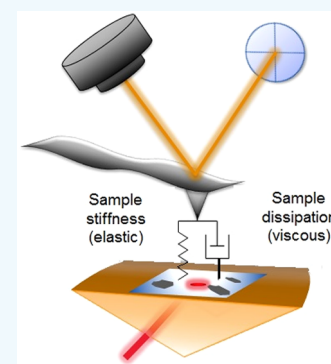
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S Supporting Information

ABSTRACT: The characterization and the optimization of packaging materials require accessing their composition with nanometric precision. A possible solution comes from atomic force microscopy–infrared spectroscopy (AFM–IR), capable of acquiring IR spectra with a spatial resolution surpassing the limit of infrared spectroscopy by far. Differentiating polyolefins, a typical component of packaging films, is complicated by the large similarity in the infrared response of this class of materials. Here, we propose a method with which to improve domains differentiation based on the analysis of IR spectra and viscoelastic properties, extracted via a routine similar to that employed in contact-resonance AFM.



KEYWORDS: polymers, AFM–IR, subdiffraction resolution, photothermally induced resonance

Assembling several layers of different polymers or polymer blends is a robust method for fabricating packaging films with excellent mechanical and barrier properties. Further improvements are achieved by dispersing organic and inorganic fillers within the polymer layers, which yields a neat reduction in production costs and allows the fine-tuning of the opacity of the protective films. Because the final performance of these hybrid materials depends on a large number of parameters, e.g., the morphology of the different phases, the thickness (approximately a few hundreds of nanometers), and the composition of the single layers and the width of the interfaces, the use of several advanced techniques is commonly required.

A robust solution for the characterization of multilayers could come from atomic force microscopy–infrared spectroscopy (AFM–IR), an emerging analytical tool that allows us to combine morphological analysis via atomic force microscopy and composition by means of infrared spectroscopy in one compact setup.^{1–3} IR spectra are obtained via a photothermally induced resonance (PTIR),⁴ relying on the mechanical detection of the thermal expansion induced in the sample by the absorption of infrared light.

Living cells,⁵ viruses and bacteria,^{6,7} polymers,⁸ quantum dots,⁹ plasmonic nanostructures,¹⁰ metal–organic frameworks,¹¹ tissues,¹² and perovskite photovoltaic devices¹³ are a few examples of the large class of materials that have already been investigated with this technique. With a penetration

depth exceeding $1\ \mu\text{m}$ ^{14,15} and a spatial resolution of $\sim 20\ \text{nm}$,¹⁶ well below the diffraction limit of the IR beam ($\sim 5\ \mu\text{m}$), AFM–IR could soon become a standard technique that allows the reverse engineering of multilayer films.¹⁷

One crucial limitation of the technique, however, severely retards the achievement of this goal: because the IR spectra of polyolefins, the major components of packaging films, are very similar, differentiation of the specific polymers remains challenging. In this regard, Tang et al. have recently proposed to differentiate polypropylene and polyethylene-co-propylene domains by implementing a calibration curve obtained via conventional FTIR in the analysis of AFM–IR data.¹⁸ Such a method, although it is affected by large uncertainties (a standard deviation of $\sim 14\%$ and a relative error of $\sim 20\%$), permitted a differentiation between PP matrix and part of the nanoscale inclusions.

Here, we introduce an analytical methodology, based on the measurement of viscoelastic properties, to improve differentiation of polyolefins via AFM–IR. Our method exploits the huge impact on mechanical properties induced by small variations in co-monomer contents. We extract a mechanical response from the time dependence of the IR signal at the cantilever and sample contact, allowing the nanometric spatial

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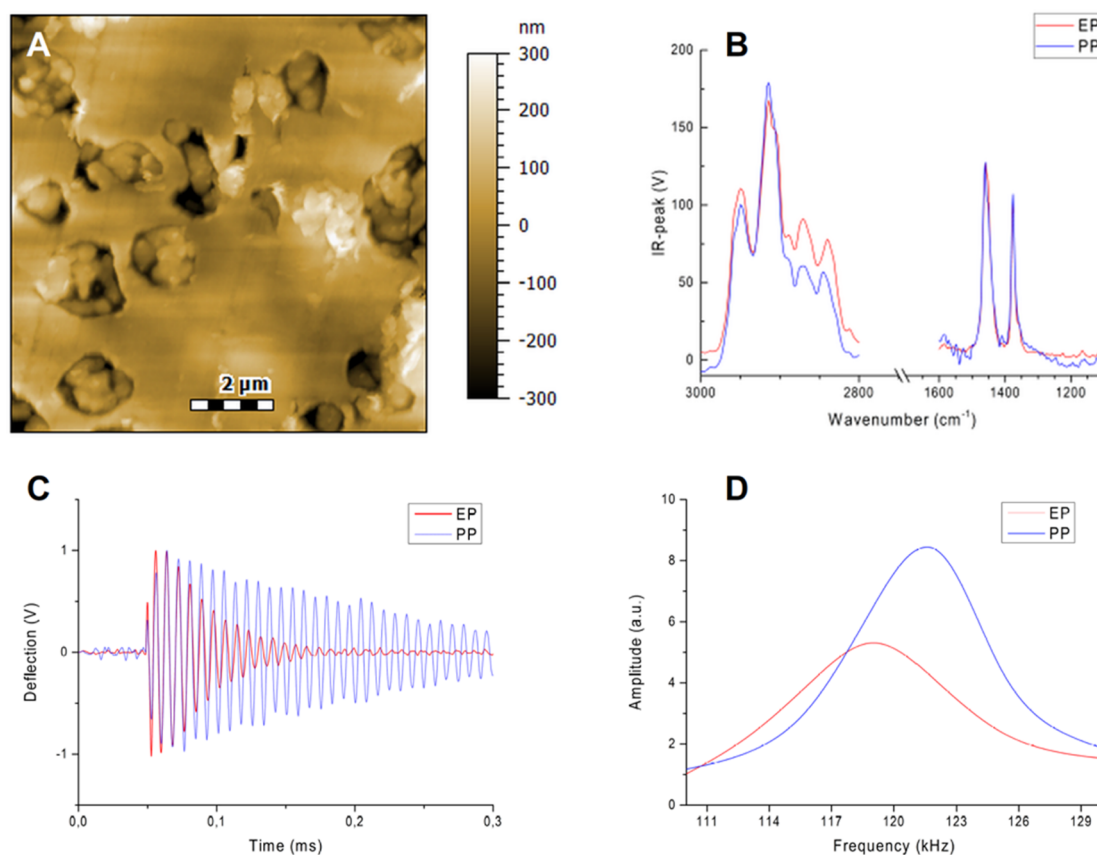


Figure 1. (A) Topography image, at constant load, of a cross-section of ICP obtained with the ThermoLeVer. The colored circles indicate the locations (blue for PP and red for EP) of the acquisition done at 1460 cm^{-1} with a laser power of 10% (B) AFM-IR spectra at the two locations. (C) Deflection signal (IR peak). (D) FT of the deflection signals (IR amplitude).

69 resolution of components having almost-identical IR spectra.
 70 Our strategy is based on the contact resonance (CR-AFM)
 71 technique,¹⁹ a standard AFM working mode, in which the
 72 cantilever oscillates in contact with the sample while scanning
 73 over the surface; see Figure 1. To understand how the
 74 cantilever interacts with the polymer surface, we considered an
 75 equivalent mechanical circuit widely used to reproduce the
 76 viscoelastic response of polymers, corresponding to a viscous
 77 damper in parallel with an elastic spring (the Kelvin–Voigt
 78 model).²⁰

79 The analysis of resonances in the amplitude of the deflection
 80 induced in the tip allows the extraction of information
 81 regarding the viscoelastic properties of the surface. A shift in
 82 the resonance frequency of the cantilever provides information
 83 on the sample stiffness, parametrized via the elastic constant of
 84 the spring considered in the Kelvin–Voigt model. The energy
 85 dissipation or damping is, instead, proportional to the quality
 86 (Q) factor of the resonance (a dimensionless factor that
 87 describes how damped an oscillator is). The latter parameter
 88 corresponds to the amplitude of the cantilever at the resonance
 89 frequency or, equivalently, to the full width at half height of the
 90 resonance peak. A quantitative characterization of viscoelastic
 91 properties with nanometric resolution is, hence, possible by
 92 simply fitting the value of resonance peaks found for each
 93 position (pixel) scanned on the surface of the sample to a
 94 simple mechanical model.

95 Considering the large analogy between PTIR and CR-AFM,
 96 we expect that AFM-IR could also be used to probe physical
 97 properties and molecular properties down to the nanoscale

level. Although full achievement of this goal would require the
 introduction of a more robust theoretical framework, we
 propose here that the sensitivity of AFM-IR to mechanical
 properties could be exploited to differentiate materials domains
 having almost-identical IR spectra.

To verify our claims, we considered a copolymer of
 polypropylene (ICP) composed of a rigid matrix of
 polypropylene (PP) with ethylene–propylene rubber (EPR)
 inclusions. Investigation via traditional IR spectroscopy of this
 material, commonly used in packaging films, would not allow
 the mapping of the distribution and the size of the different
 domains because those are well below the diffraction limit.

In AFM-IR, similar to an attenuated total reflection (ATR)
 setup, the IR beam here reflects on the sample sitting on a
 ZnSe prism with a pulse of 12 ns, at the rate of 1 pulse per
 millisecond. The induced evanescent wave diffuses across the
 whole polymer layer, which rises the temperature and, hence,
 increases the sample thickness. Because the tip was already in
 contact with the sample, the sudden change in the height of the
 surface induces an instantaneous deflection in the cantilever.
 This excitation eventually decays upon interaction with the
 polymer layer and provides a straightforward way to probe the
 viscoelastic properties of the surface. Although we used a
 conventional tip with relatively low characteristic resonance
 frequency (120.5 kHz),²¹ the measurement is not affected by
 time-dependent variations in the surface height, decaying at the
 time scale of heat relaxation ($\lesssim 1\ \mu\text{s}$). We remark that in the
 case of AFM-IR, the deflection signal does not convolute with

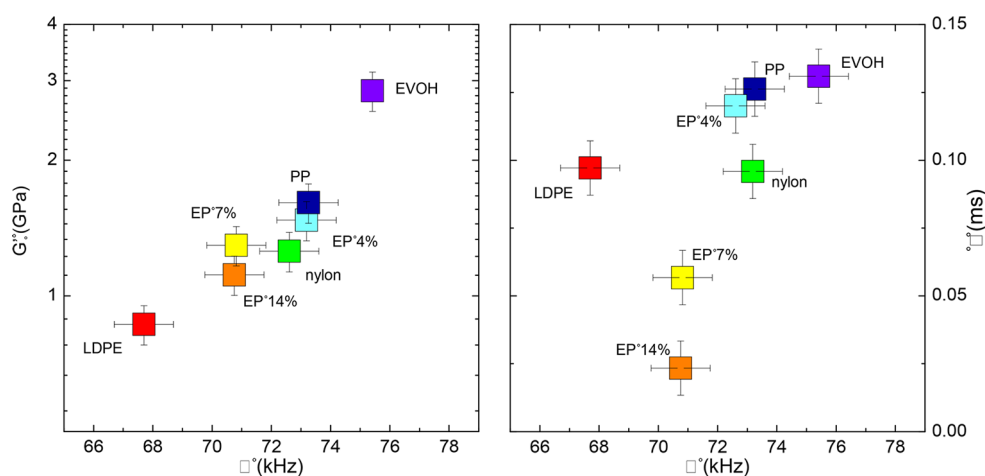


Figure 2. Left panel shows the correlation between the frequency and the storage modulus G' at 223 K. Data were obtained at 1460 cm^{-1} with a contact tip from Anasys Instruments and with a load force of 37.5 nN. The right panel shows the differentiation of materials with close frequencies based on the decay time. Data were obtained at 1460 cm^{-1} with a contact tip from Anasys Instruments and with a load force of 37.5 nN.

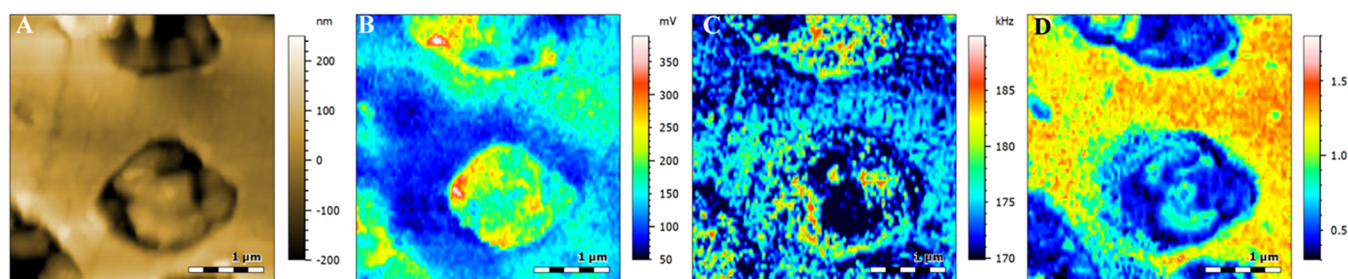


Figure 3. Images of a cross-section of ICP obtained with the ThermoLever. (A) Topography image. (B) IR peak map. (C) Resonance frequency map. (D) Map of the dimensionless ratio I_ω/A_0 , where I_ω is the amplitude of the Fourier-transformed IR signal at its resonance frequency and A_0 is the deflection at zero time. The maps were obtained at 1460 cm^{-1} with a laser power of 8% at an acquisition rate of 0.05 Hz with a pulse co-averaging of 32 scans.

126 thermal expansivity because its off-resonance sensitivity is
127 low.²²

128 The deflection in the cantilever with respect to the surface
129 can be described as the sum of damped harmonic oscillators of
130 the following type:²³

$$S = A_0 \cos(\omega t) \exp\left(-\frac{t}{\tau}\right) \quad (1)$$

132 where A_0 is the deflection at zero time, ω is the frequency of
133 the selected (a pass-band filter was used) eigenmode, and τ its
134 characteristic decay time. ω is directly related to the shift in
135 frequency of the cantilever and, thus, to the stiffness of the
136 sample (parametrized, for example, by the elastic modulus G'),
137 while τ provides information on the viscous character of the
138 material (loss modulus G''). In fact, the Fourier transformation
139 of the expression in eq 1 provides a Lorentzian function
140 centered at ω . The value of τ can be straightforwardly obtained
141 as $(a\pi)^{-1}$, where a is the full width at half height of the
142 transformed signal,¹³ related to the damping component of our
143 mechanical circuit.

144 Figure 1A shows the topography image obtained in contact
145 mode on a section of ICP, where inclusions of EPR, darker on
146 the image, are dispersed in the PP matrix. In Figure 1B, we
147 report the damped oscillating signals (deflection in the
148 cantilever with respect to the surface) measured on the
149 polypropylene matrix and on the ethylene-propylene
150 inclusion; the corresponding Fourier-transformed signals are
151 plotted in Figure 1C. Although both polymers have the same

maximum starting amplitude (A_0), the oscillations in the EP 152
domain decays much faster than in the PP matrix. The first 153
observation implies that the two polymers experienced a 154
comparable change in volume upon thermal expansion, while 155
the latter indicates that the EP inclusions dissipate more 156
efficiently the thermal impulse, consistent with the rubbery 157
character of this polymer. 158

To complete the validation of our claims, we performed an 159
additional set of experiments in which we measured via 160
dynamic mechanical thermal analysis (DMTA) the mechanical 161
properties of different commercial polymers. Based on the 162
work of Yablon et al., the Q-factor and the resonance frequency 163
are a probe of the viscous and elastic mechanical response.²⁴ 164
To quantify these parameters, we measured the temperature 165
and frequency response of the storage and loss modulus (G' 166
and G''). We expect a direct correlation between ω , the shift in 167
frequency of the cantilever, and G' (elastic response) and 168
between G'' and τ because both quantities provide information 169
regarding the viscous character of the material. 170

Although we could not reach via DMTA the high resonance 171
frequency used in AFM-IR, simple considerations allowed us 172
to compare the results obtained via the two experimental 173
methods. AFM-IR was operated at room temperature at 70 174
kHz, associated with a characteristic time of $\sim 2\text{ }\mu\text{s}$. In these 175
conditions, all of the polymers investigated are in the glassy 176
state and exhibit an unrelaxed mechanical solid-like response. 177
This regime corresponds to a high modulus plateau in G' 178
coupled to zero loss ($G'' \simeq \partial G'/\partial \log \omega$, an approximation 179

180 valid for all the dynamic complex functions owing to the
181 Kramers–Kronig relation), as observed at low temperatures in
182 isochronal conditions. Because of the lack of material
183 dependence on the intrinsic value of G'' at low temperatures
184 and high frequency, the comparison between viscoelastic
185 properties and IR signal can be performed only for G' . We
186 considered 223 K, the lowest temperature achievable by the
187 DMTA setup, in which each analyzed polymer is in the glassy
188 state. In Figure 2, we plotted the values of ω (see eq 1)
189 measured via AFM–IR, as a function of the values of G' . The
190 excellent correlation between two independent data sets
191 validate our claims on the sensitivity of AFM–IR on nanoscale
192 mechanical properties.

193 Despite the lack of correlation with G'' , the decay time τ can
194 be used to differentiate materials whose characteristic
195 frequency ω is too close. Analysis of τ can be, hence,
196 employed to overcome possible limitations of our method due
197 to G' values that are too similar. In the left panel of Figure 2,
198 we show that the elastic moduli of PP and EP 4% are identical
199 within experimental errors; therefore, differentiating PP and
200 EP by ω is not possible. On the contrary, the decay time of
201 those materials differs significantly; see the right panel of
202 Figure 2. The differentiation of polypropylene and poly-
203 ethylene-*co*-propylene is, therefore, possible based on the decay
204 time.

205 With these ideas in mind, in Figure 3, we show an example
206 of analysis of the same material used in Figure 1. Contrast in
207 the topography image (Figure 3A) is ensured by the different
208 elastic modulus of the two components. Scanning at constant
209 force results in apparently lower heights for softer domains,
210 where the tip can penetrate deeper. Consequently, EP domains
211 appear darker. This effect convolutes with IR absorption in a
212 traditional IR map (Figure 3B), which reduces contrast
213 between the different polymers. A more-accurate differ-
214 entiation of the domains is obtained by mapping the resonance
215 frequency (Figure 3C) or a dimensionless parameter given by
216 the ratio of the maximum amplitude of the Fourier-trans-
217 formed IR signal and the intensity of the deflection at zero
218 time (Figure 3D). This parameter, proportional to the line
219 width and inversely proportional to the decay time, was build
220 up to further exploit the contrast arising from the large
221 difference in the mechanical behavior of the two polymers.

222 We are confident that our viscoelastic analysis will be widely
223 employed, in combination with IR signatures, to achieve a
224 more-accurate analysis of polymer components in packaging
225 films and other devices. We hope that our experimental data
226 will stimulate discussion in the community and promote the
227 development of a valid theoretical framework with which to
228 obtain quantitative viscoelastic information via AFM–IR
229 measurements.

230 ■ ASSOCIATED CONTENT

231 ⓘ Supporting Information

232 The Supporting Information is available free of charge on the
233 ACS Publications website at DOI: 10.1021/acsapm.8b00243.

234 Experimental protocol followed for AFM–IR and
235 DMTA measurements (PDF)

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Notes

The authors declare no competing financial interest.

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